James River Water Quality Model Refinement and Scenario Runs

Progress Report

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Outline

- Progress update
- Theoretical consideration under nutrient-limited condition
 - Parameter uncertainty
 - Model response to load reduction
- Model calibration results
- Model response to load reduction
- Discussion

Progress Update

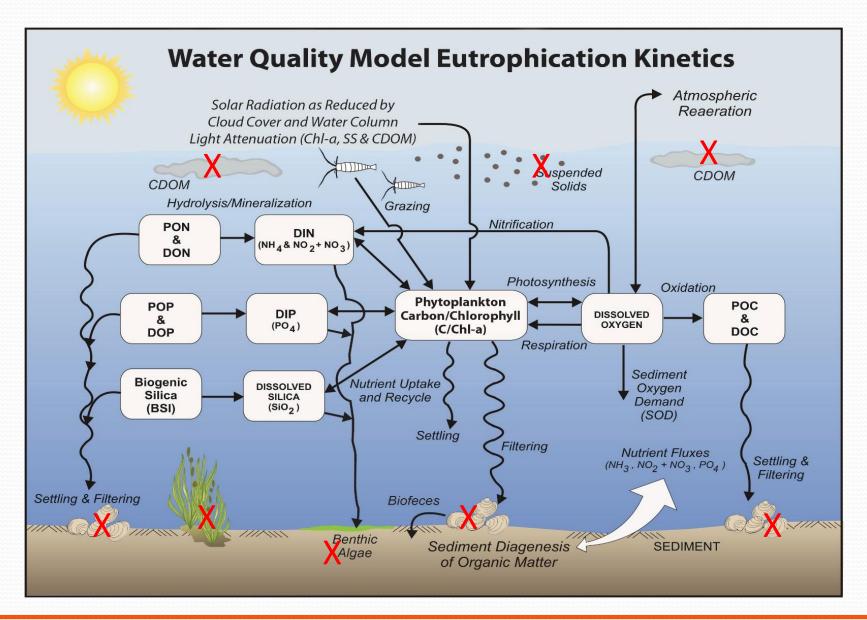
- Received data
 - latest Phases 6 watershed nonpoint source model results 1985-2014 (nonpoint/point, bank erosion, atmospheric deposition)
 - Draft WIP2 scenario 1985-2000
 - Boundary conditions (tide, salinity, temperature)
- Completed tools to convert data to EFDC inputs
- Conducted model calibration
 - Hydrodynamics (from 1991-2013)
 - Water quality (from 1991-2013)
- Sensitivity test for model response to load reduction

Comparison of Loading to James River Watershed Loading (2016)

1991-2000	TC (Mlb/yr)	TN(Mlb/yr)	TP(Mlb/yr)
Bay	156.7	36.93	4.69
DEQ (2016)	85.9	26.4	3.5
DEQ/Bay	55%	71%	75%
2006-2013	TC (Mlb/yr)	TN(Mlb/yr)	TP(Mlb/yr)
Bay	145.57	30.15	3.11
DEQ (2016)	78.4	21.2	2.49
DEQ/Bay	54%	70%	80%

Can we calibrate model to fit the observation data using different loadings?

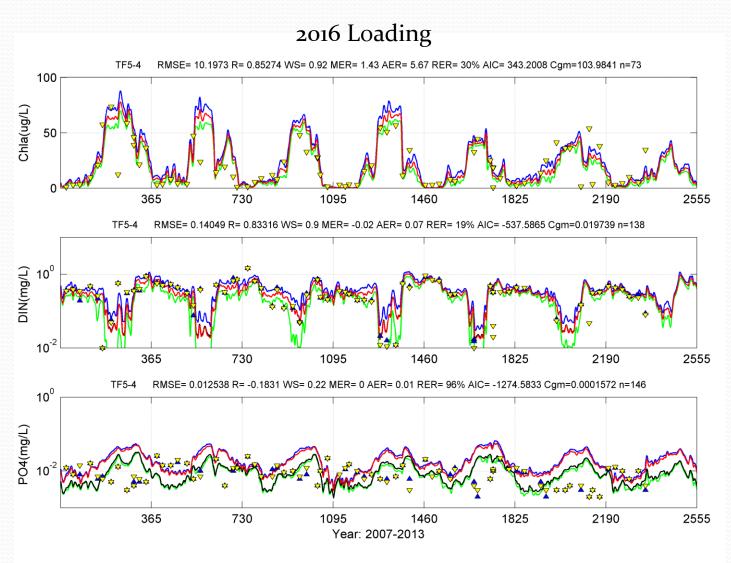
Model Kinetic Processes



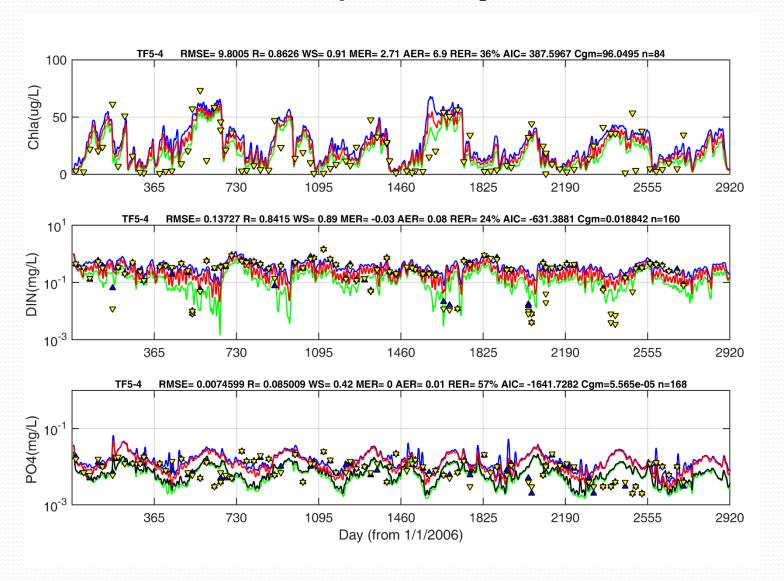
Model Configuration

- Flow and loadings use WSM daily model outputs
 - POC, DOC, PON, DON, NH4, NO23, POP, DOP, PO4, and DO
 - POC, DOC, PON, DON, POP, and DOP
- Solar radiation uses hourly observations at Norfolk and Richmond stations
- Open boundary condition
 - 1991-2000 uses Chesapeake Bay model outputs (tide, salinity, temperature, and water quality state variables
 - 2007-2013 uses observations and VIMS Bay model of salinity. Water quality state variables use interpolation of observations near the James River mouth.
- Hourly observed wind data are used for computing aeration.
- Suspended solids use spatially and temporally interpolated results based on observations.
- Initial condition for bottom sediment diagenesis model
 - Repeat simulations until dynamic equilibrium is reached.

Example of Model Calibration Using Different Loadings



Bay 2017 Loading



Consideration of a Simple System

$$\frac{\partial N}{\partial t} = L - FN - \frac{N}{N + N_h} GC + \gamma RC$$

$$\frac{\partial C}{\partial t} = \frac{N}{N + N_h} GC - RC - FC$$

Steady State

$$\frac{N}{N+N_h}GC = (R+F)C$$

L=DIN loading (mass/volume/day)

F=flushing rate

N_h=DIN half saturation rate

 γ = nutrient recycle

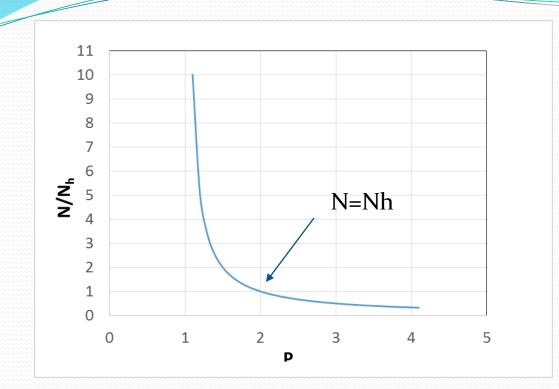
C= phytoplankton (nitrogen-based)

G= phytoplankton growth rate

R= total loss (respiration, mortality, settling)

$$\frac{N}{N_h} = \frac{R+F}{G-(R+F)} \qquad P = \frac{G}{R+F}$$

Nutrient Concentration



G=2(F+R), N=Nh

Example:
Residence time = 10 day
F=0.1
Respiration =0.1/d
Mortality =0.05/d
Settling =0.5 /d
R=0.65
G=1.3 /d

- It is possible to find a set of parameters to simulate DIN to its limiting level if nutrient is limited
- The parameter selection depends on dynamic conditions
- Parameters are correlated to each other

Phytoplankton Concentration

$$\frac{N}{N+N_h} = \frac{R+F}{G} = \frac{1}{P}$$

$$C = \frac{L - FN}{(1 - \gamma)R + F}$$

Assume load L is reduced to kL (k<1)

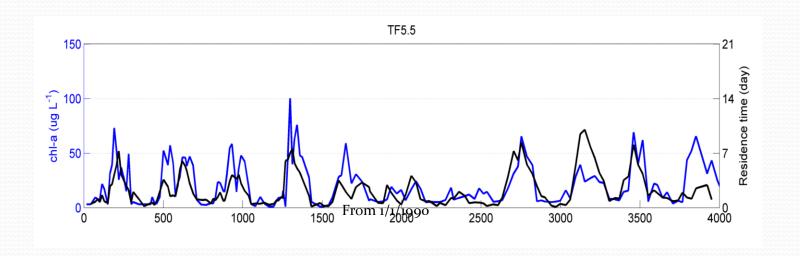
$$C1 = \frac{kL - FN}{(1 - \gamma)R + F}$$

$$C - C1 = \frac{(1-k)L}{(1-\gamma)R + F}$$

$$\frac{C - C1}{C} = \frac{(1 - k)L}{L - FN}$$

- The results show that the response of phytoplankton reduction depends on the flushing rate (residence time τ = 1/F)
- If a model has a short residence time, the phytoplankton concentration is more sensitive to the load reduction than a long residence time model

High Correlation of Residence Time and Phytoplankton Concentration



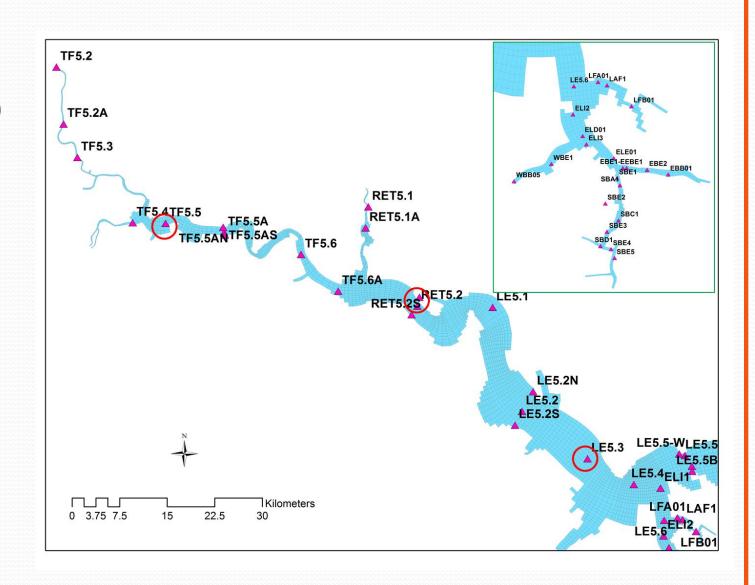
Model Results

- 2007-2013
- 1991-2000
- Stations:

TF5.1

RET5.2

LE5.3



Model Skill Assessment Criteria

- Model-data graphic comparison
 - Direct comparison
 - Scatter plots
 - Accumulative distribution
 - Error distribution
- Statistics
 - Correlation (R)
 - Root-mean-square error (ER)
 - Model Skill (SS, WS)
 - Mean error (ME)
 - Absolut mean error (AME)
 - Relative error (RE)
- Processes
 - Primary production
 - Respiration
 - Net ecosystem metabolism

$$ER = \sqrt{\frac{\sum_{k=1}^{n} (P_k - O_k)^2}{n}}$$

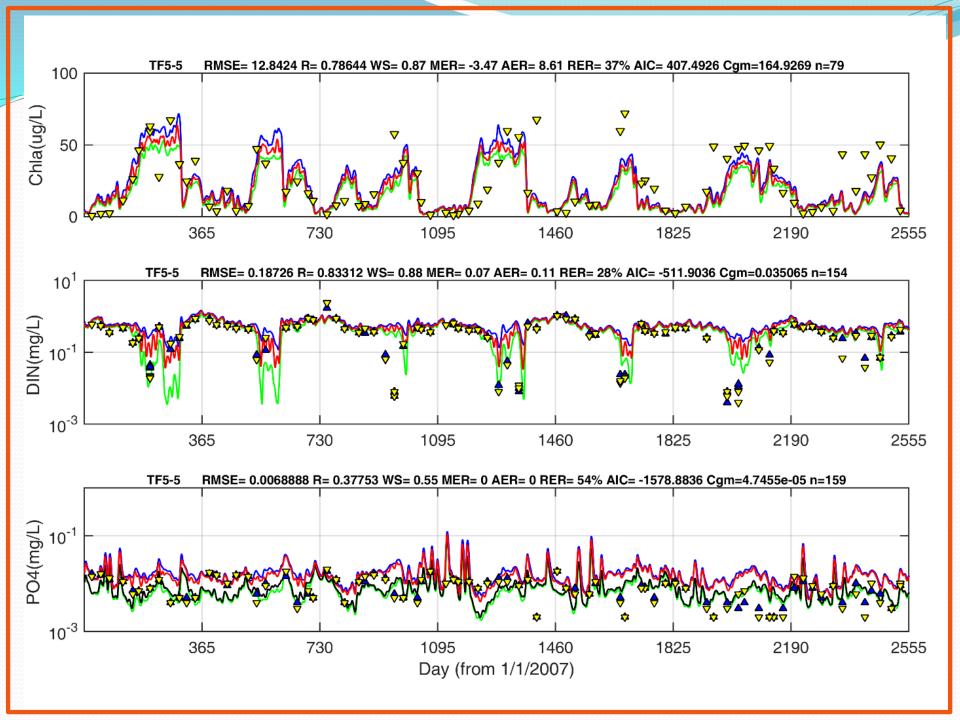
$$SS = 1 - \frac{\sum_{k=1}^{n} (P_k - O_k)^2}{\sum_{k=1}^{n} (O_k - \bar{O})^2}$$

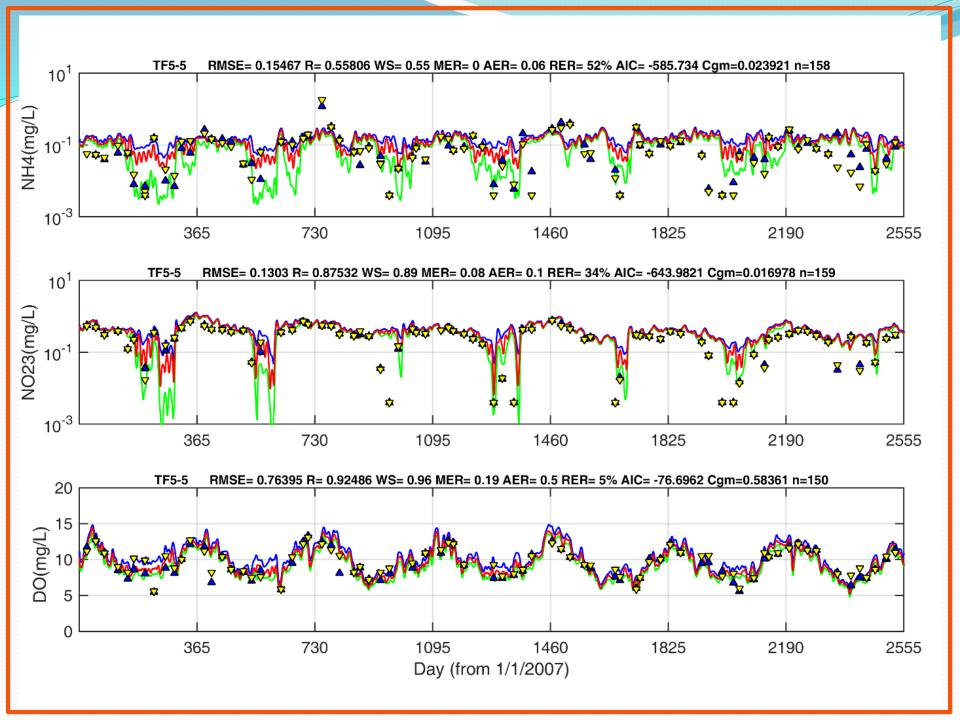
$$WS = 1 - \frac{\sum_{k=1}^{n} (P_k - O_k)^2}{\sum_{k=1}^{n} (P_k - \bar{P})^2}$$

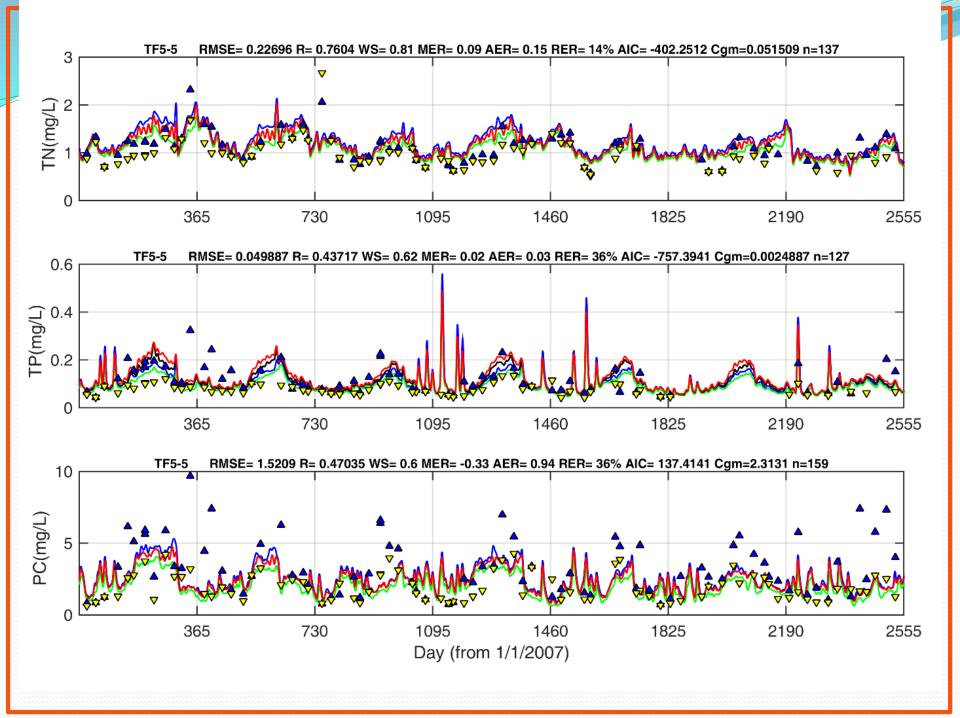
$$ME = \sum_{k=1}^{n} (P_k - O_k)/N$$

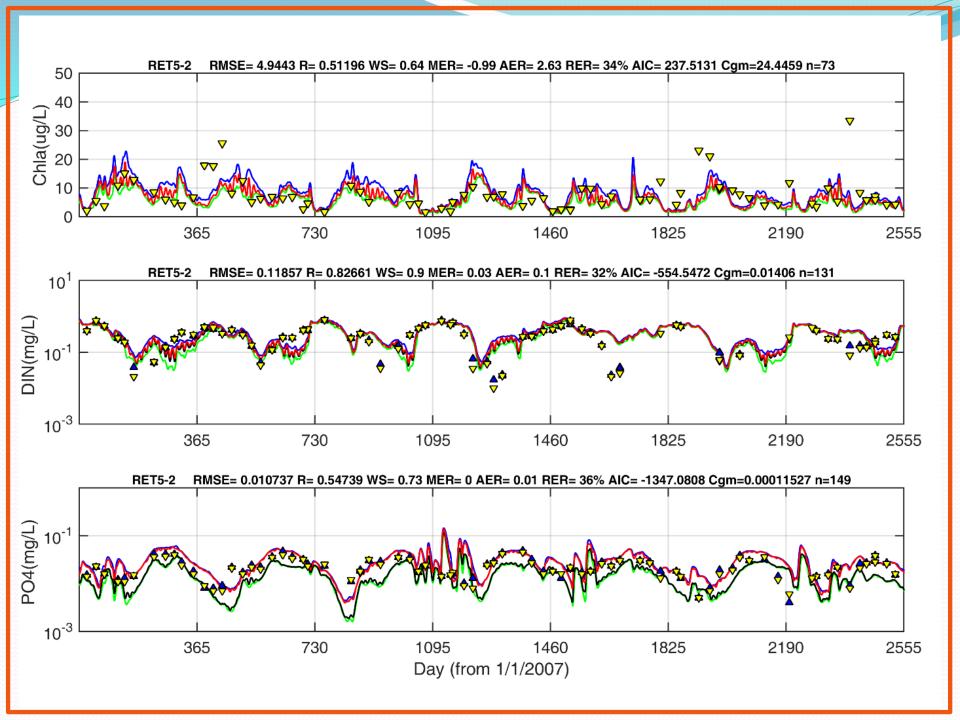
$$AME = \sum_{k=1}^{n} |P_k - O_k|/N$$

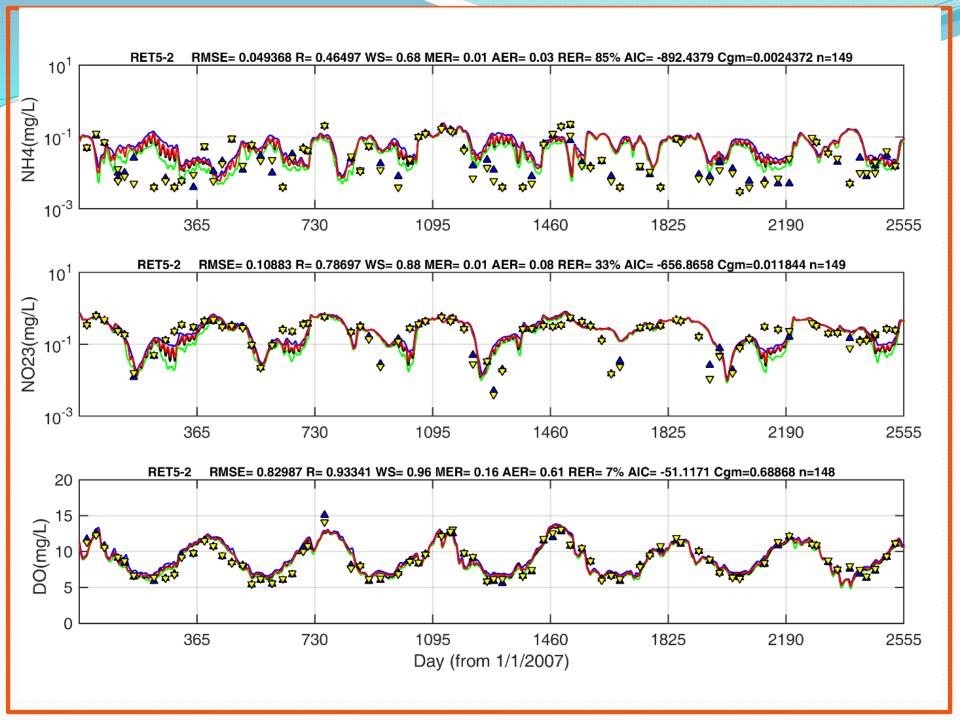
$$RE = \frac{\sum_{k=1}^{n} |P_k - O_k|}{\sum_{k=1}^{n} O_k}$$

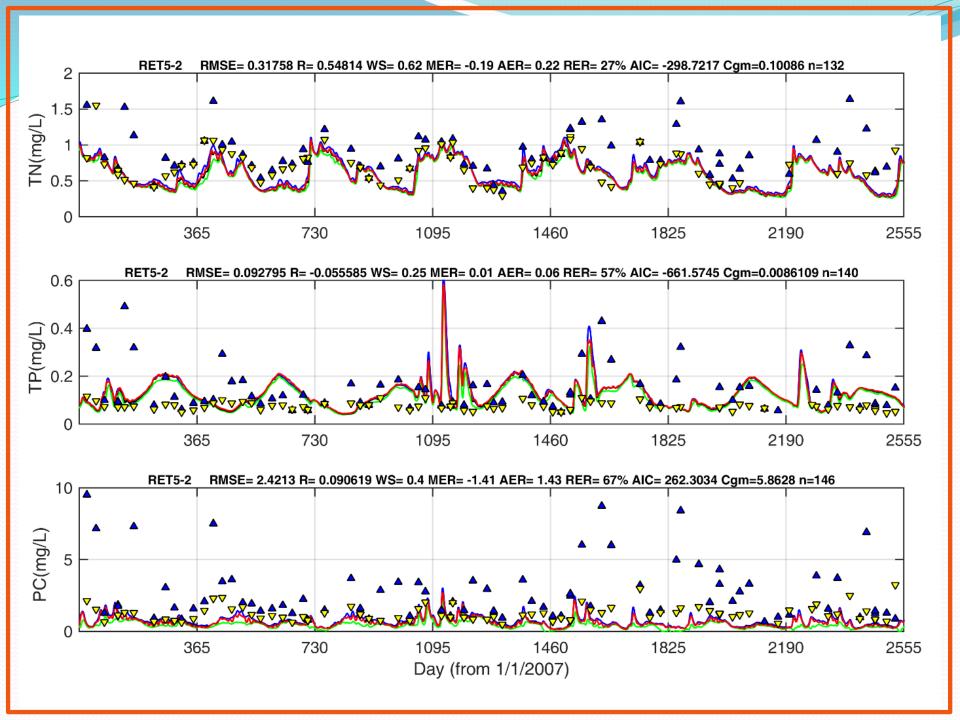


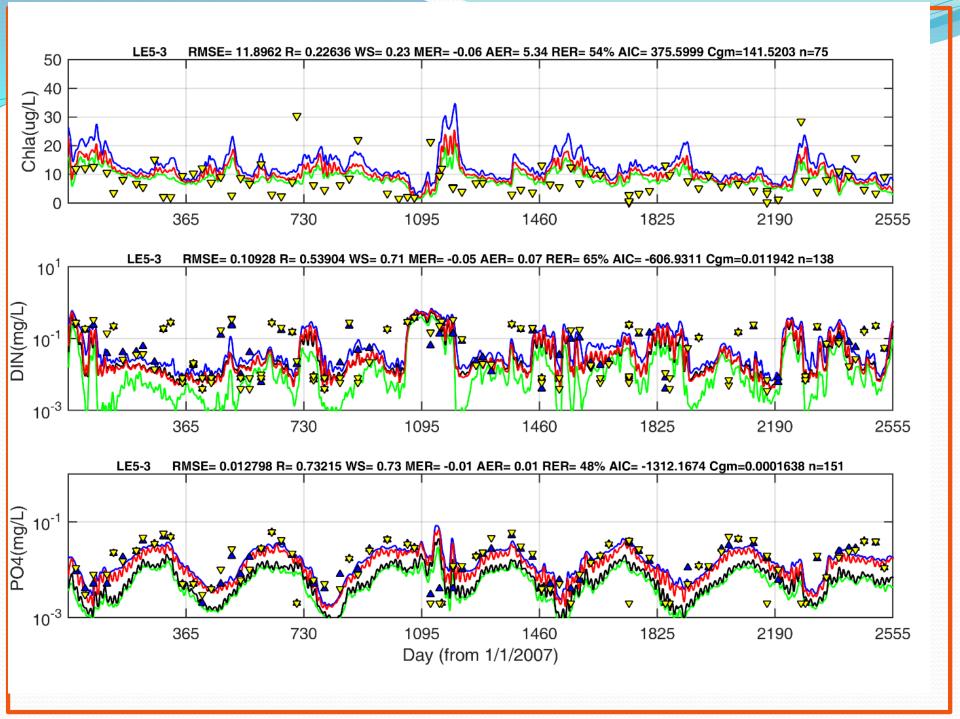


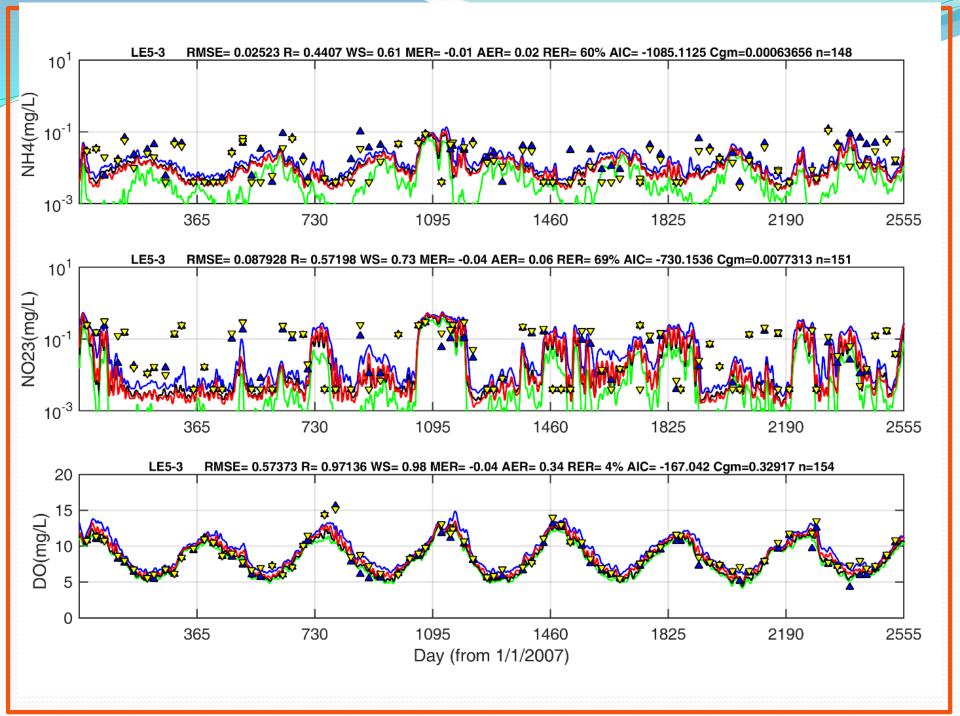


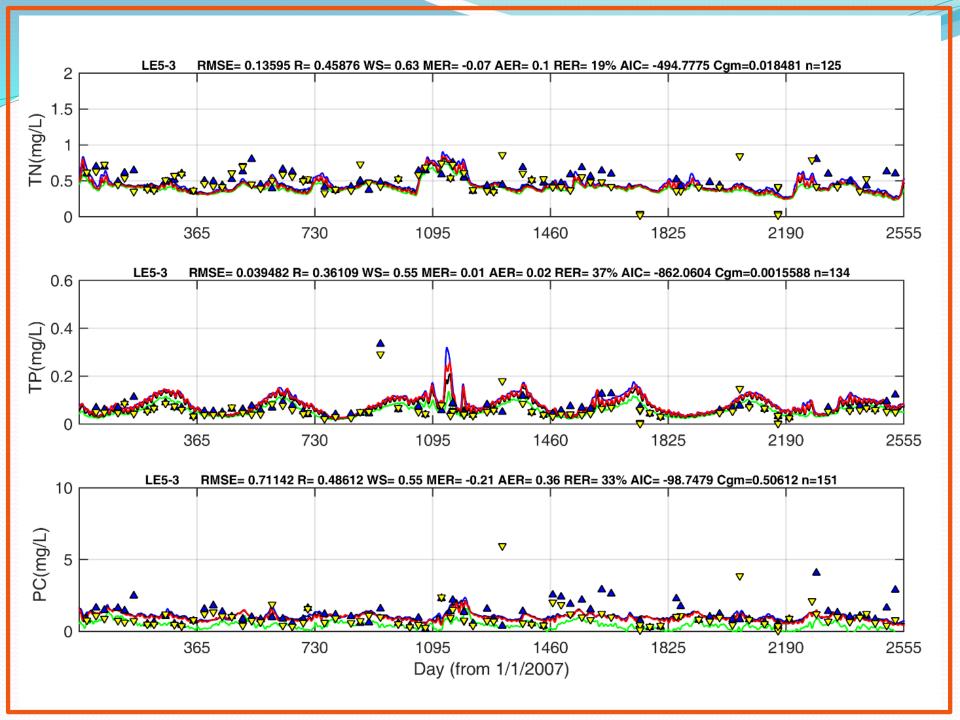


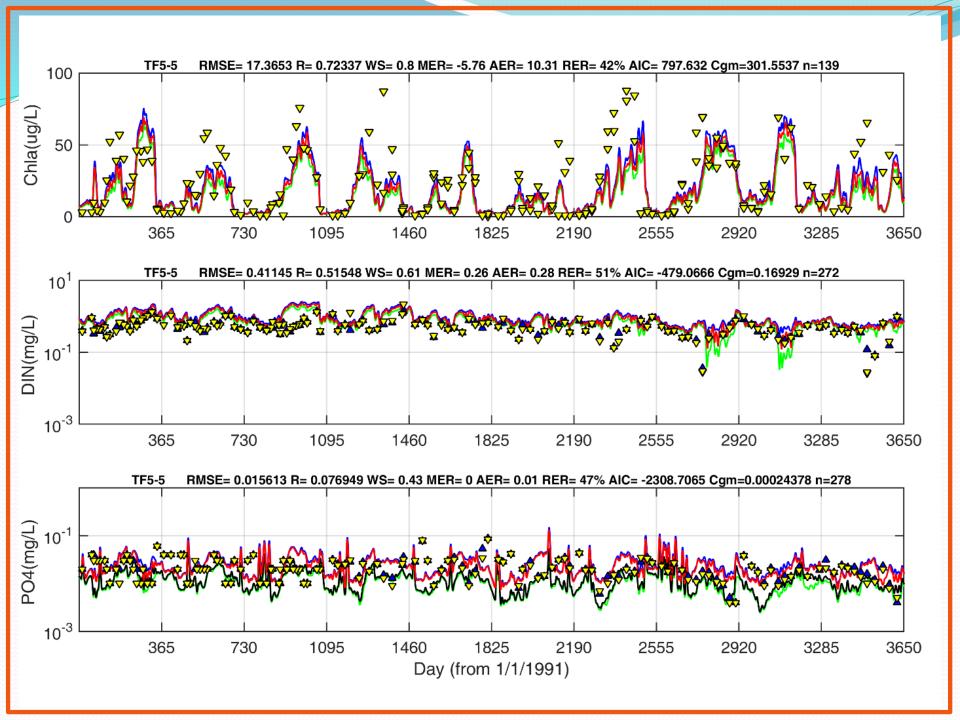


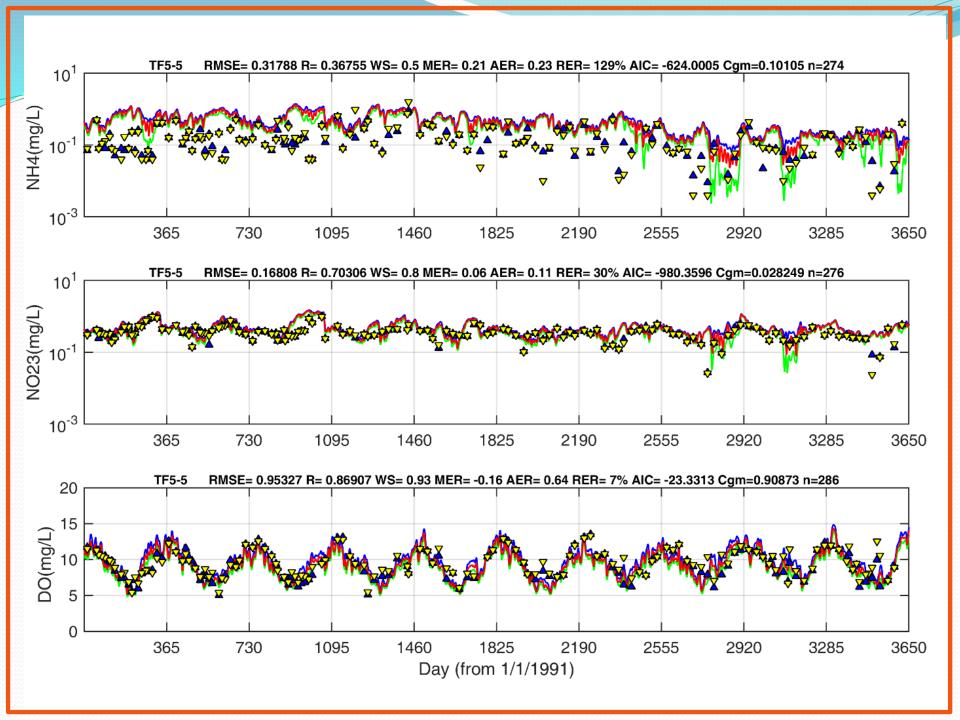


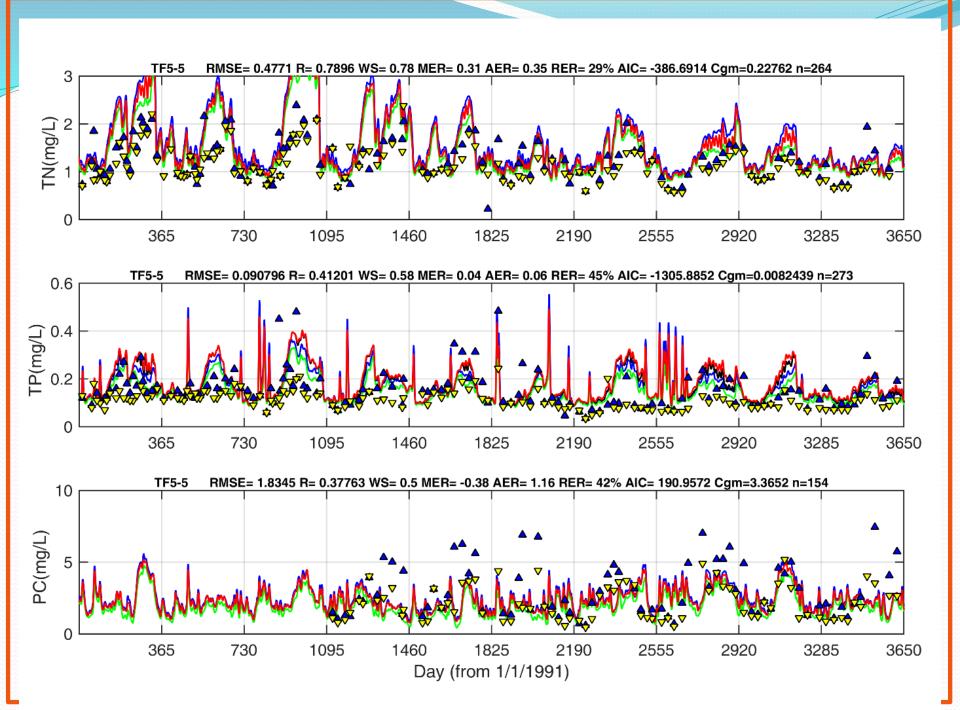


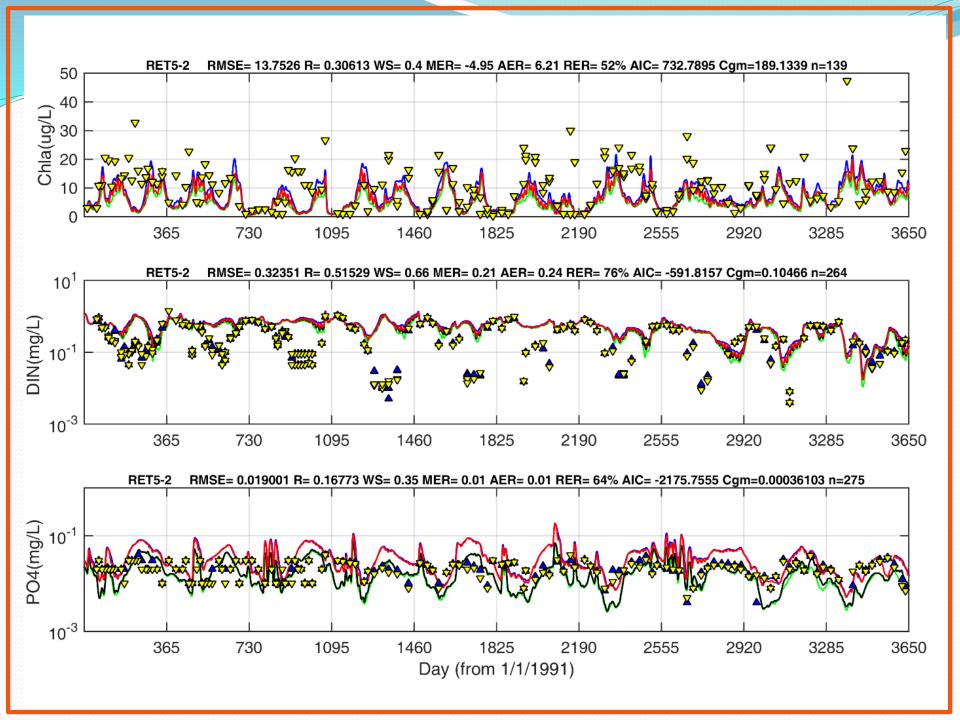


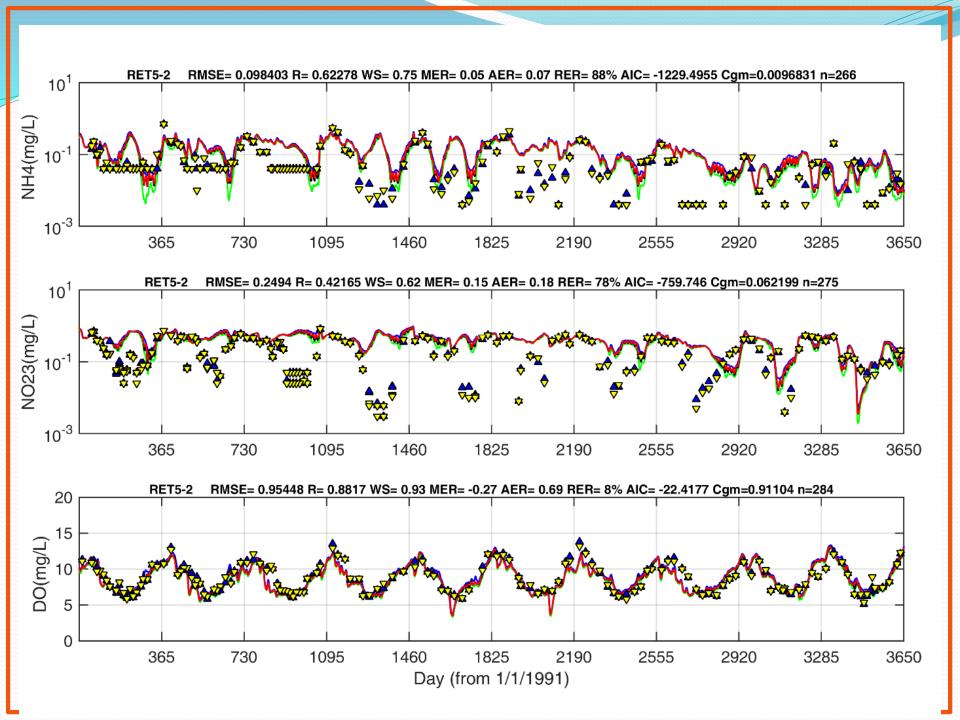


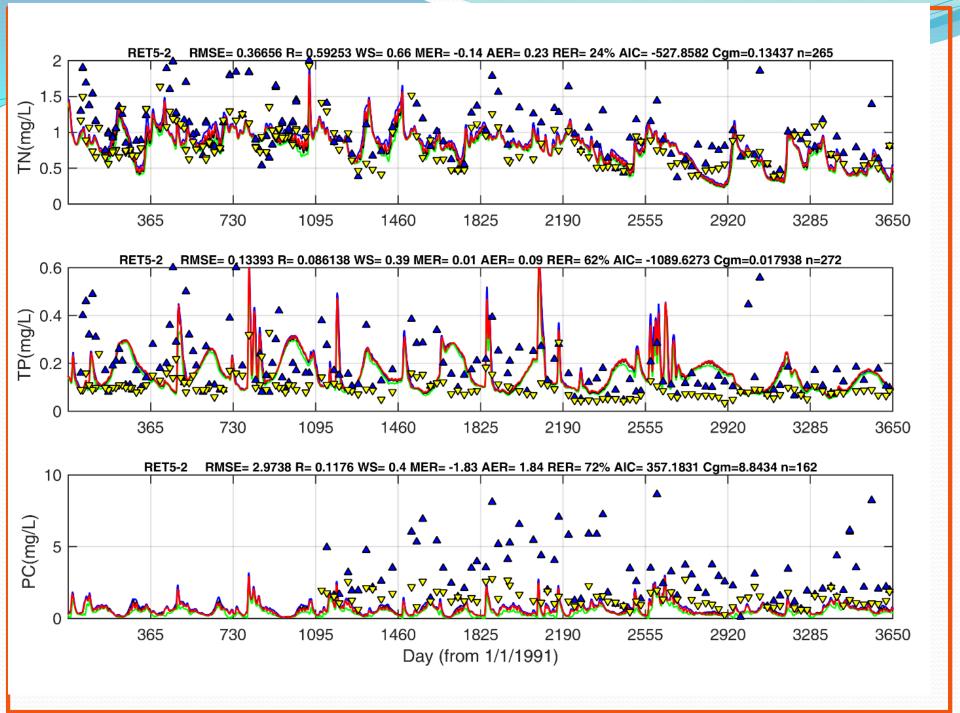


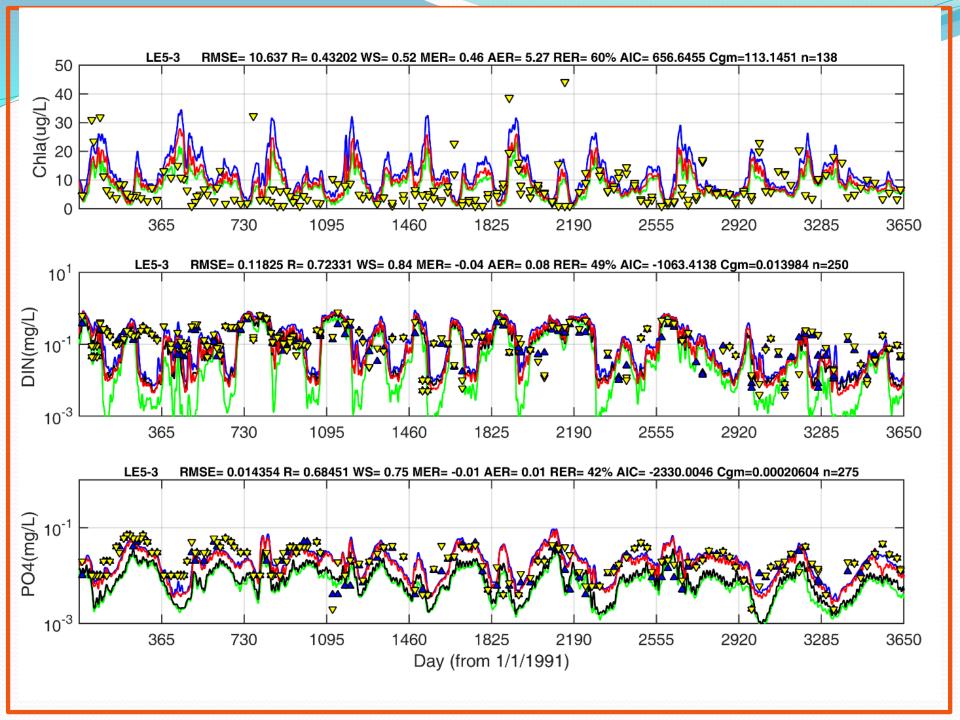


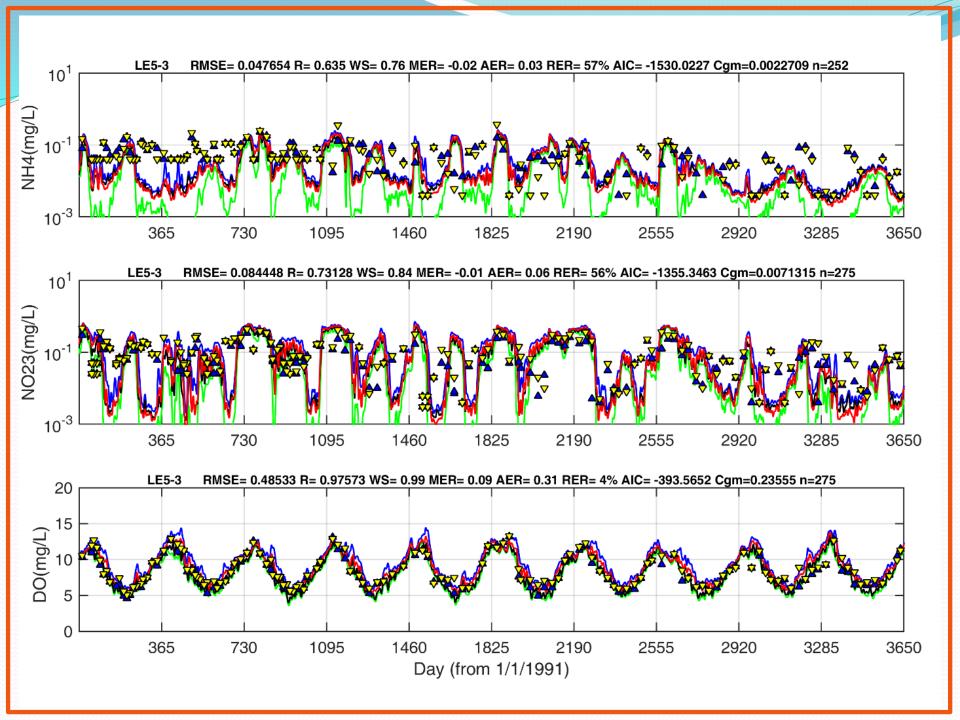


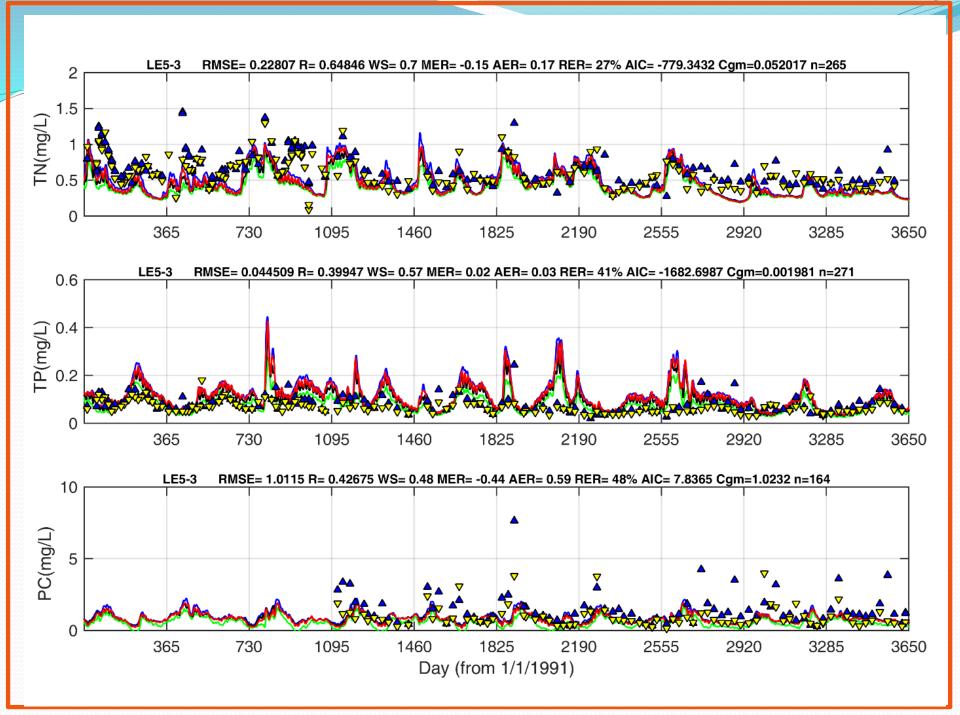




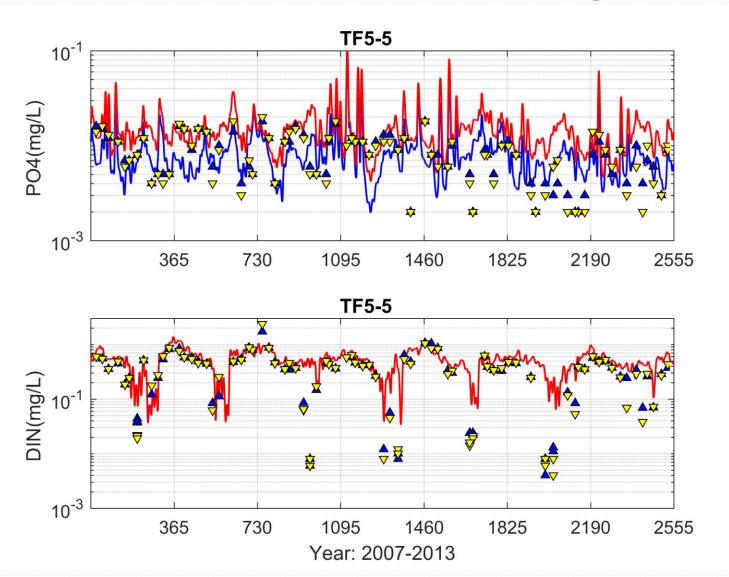


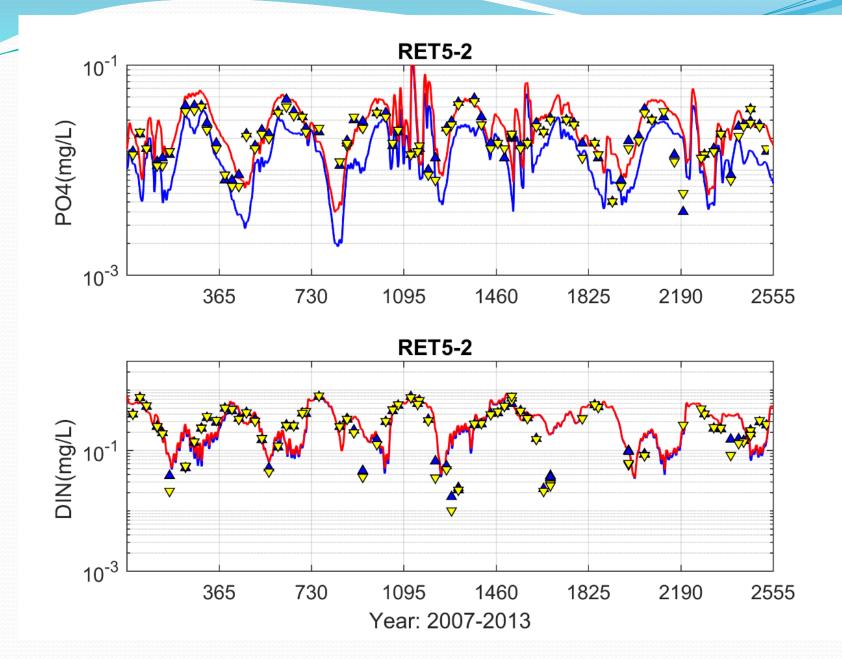


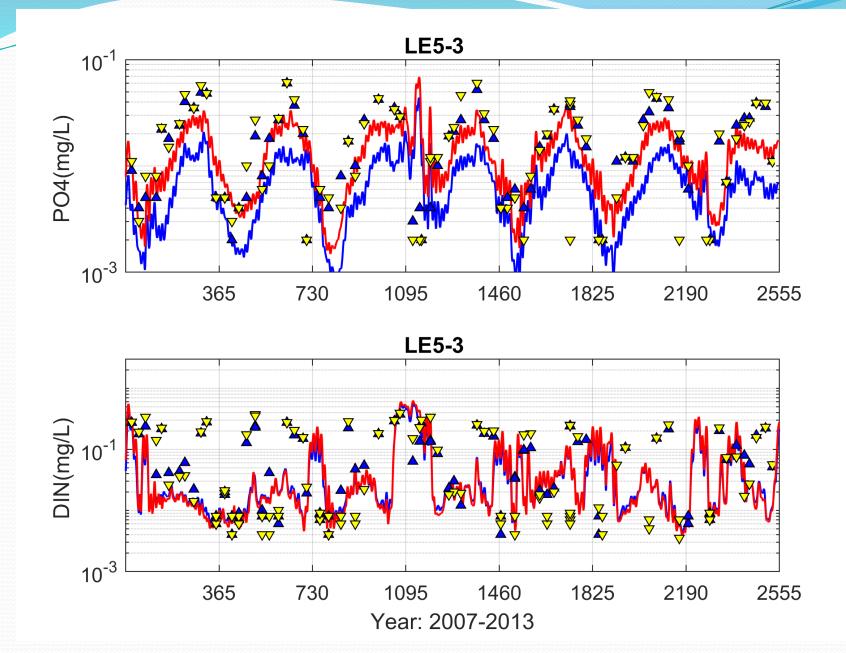




Nutrient Limiting

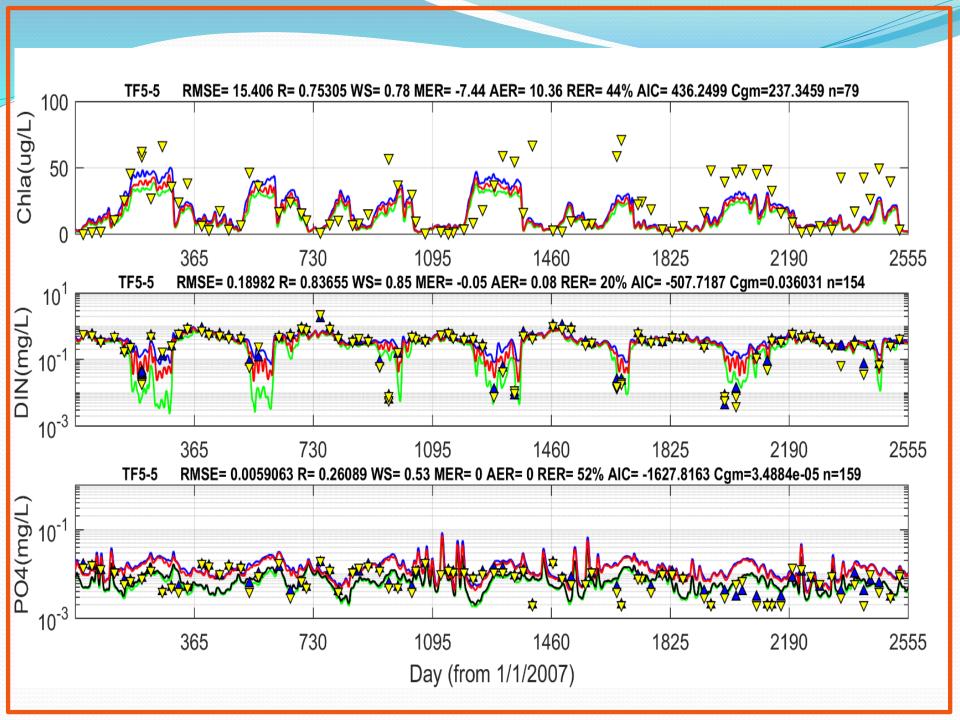


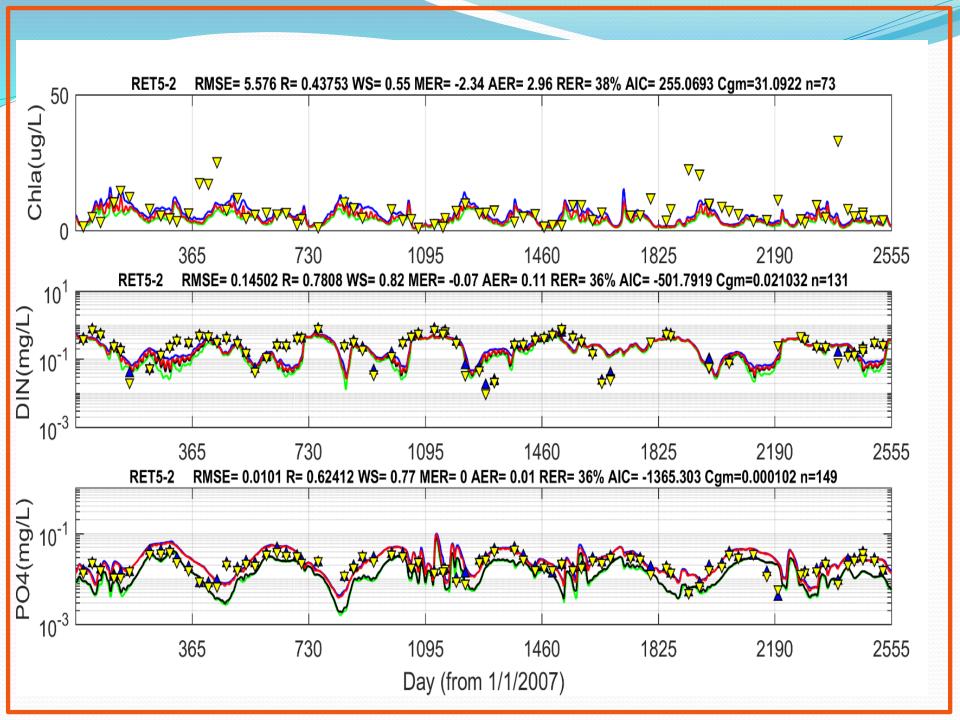


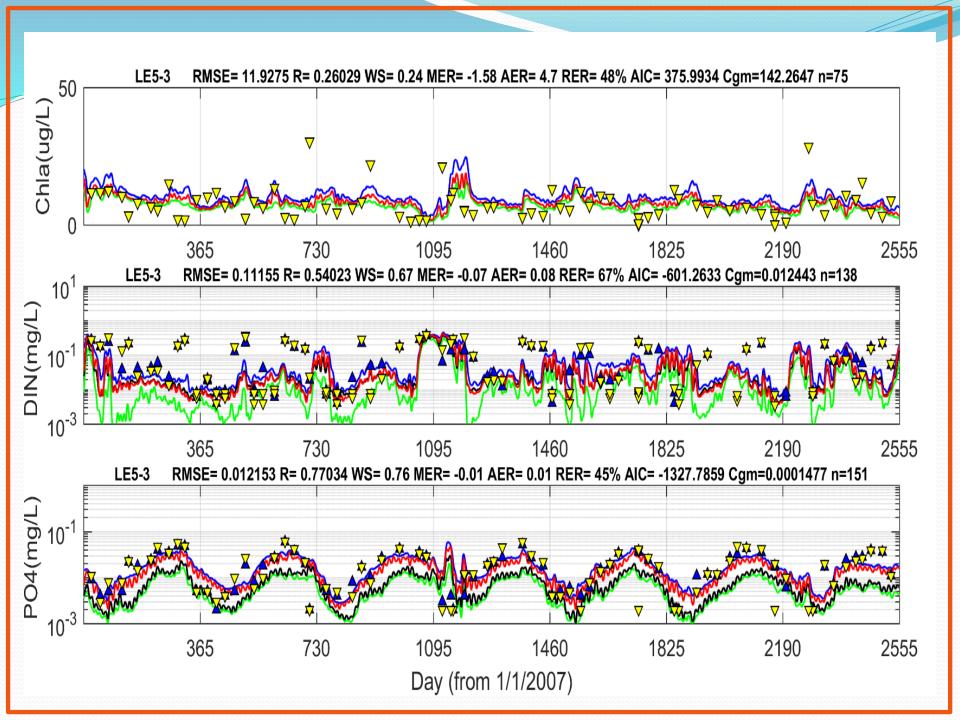


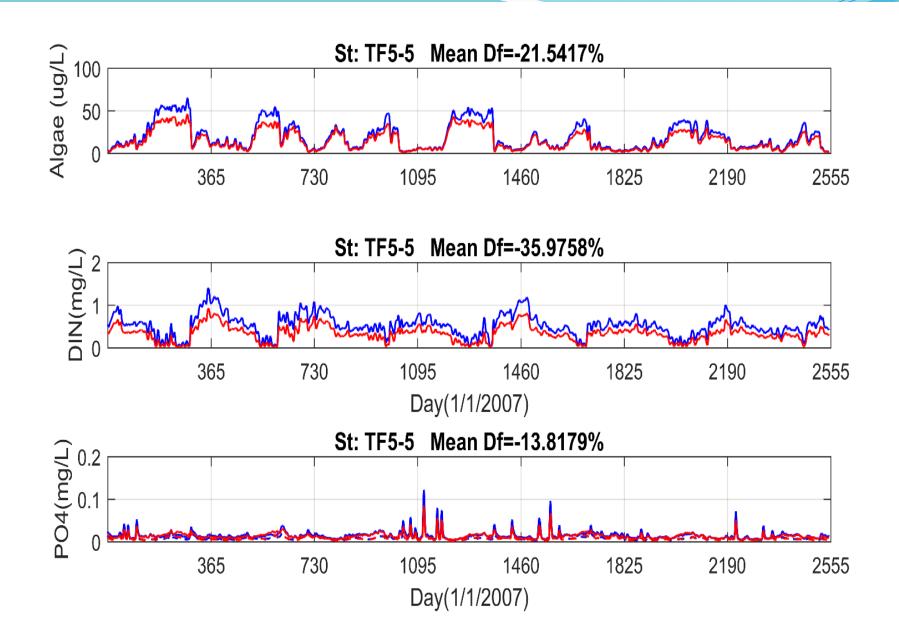
Model Response to Nutrient Reduction

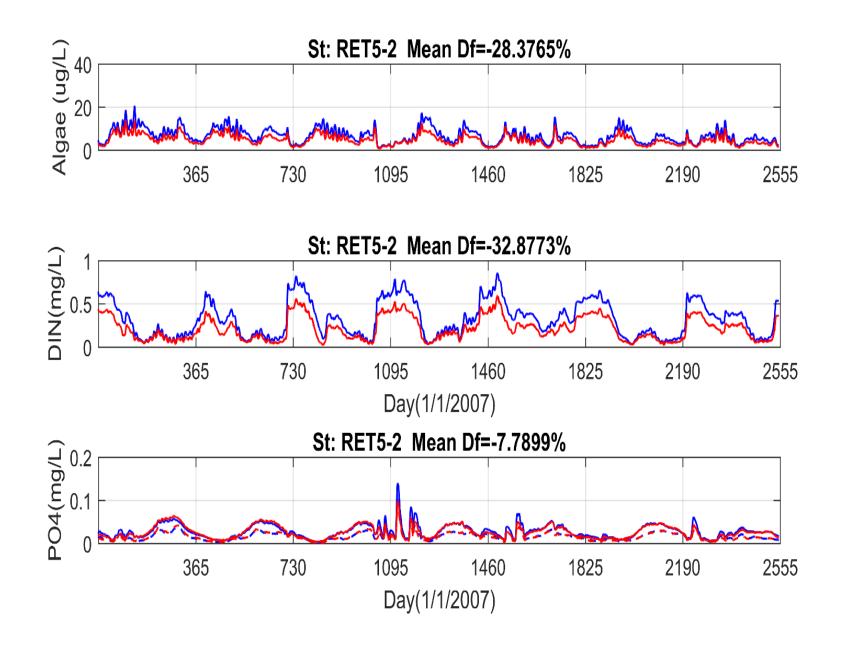
- Conduct a sensitivity test for reduction of N and P by 30% everywhere
- No reduction of phytoplankton from fall-line
- No change of boundary condition

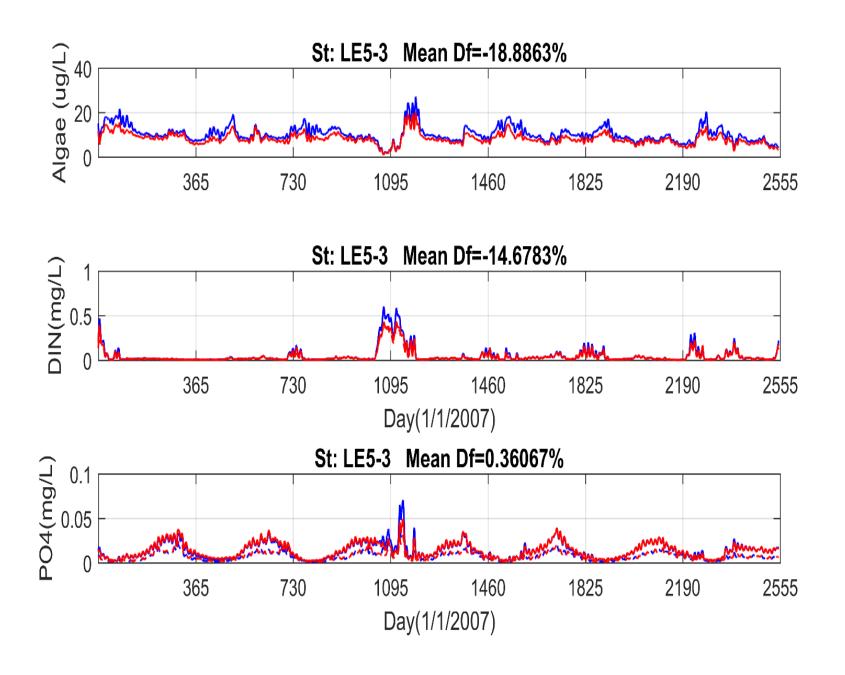




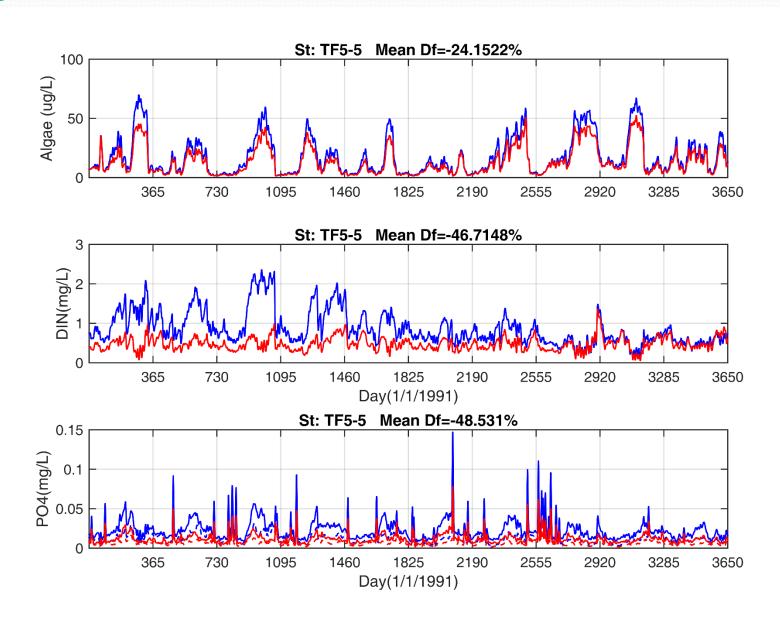


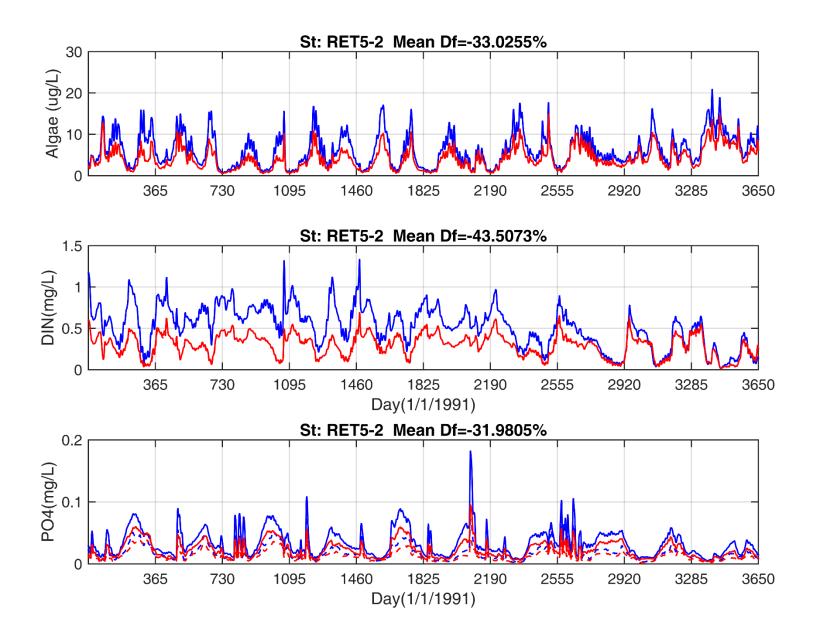


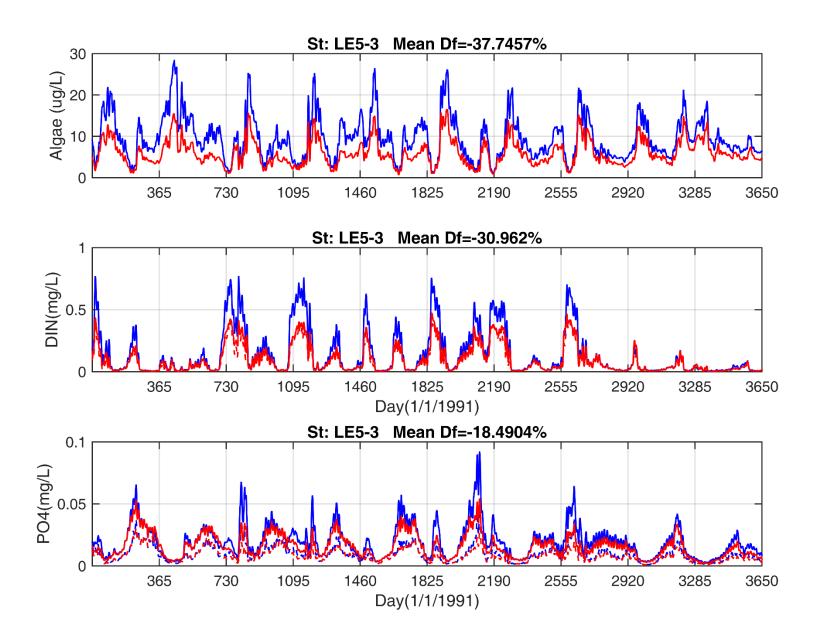




Test Draft WIP2 scenario 1985-2000







Conclusions

- Calibration of model parameters depends on the dynamic condition.
- For a nutrient limited estuary, one can use different model parameters to calibrate model for different loadings.
- The response of model to loading reduction depends on transport time. A model with a short transport time is more sensitive to load reduction than a model with longer transport time.
- The model sensitivity test of response to load reduction shows that the change of phytoplankton concentration is less than change of nitrogen concentration.
- The model is not very sensitive to phosphorus reduction, which needs to be further investigated.